

EVALUATION OF n + 60Ni CROSS SECTIONS FOR THE ENERGY
RANGE 1.0E-11 to 150 MeV

S. Chiba, M. B. Chadwick, P. G. Young, and A. J. Koning
22 Sept. 1997

This evaluation provides a complete representation of the nuclear data needed for transport, damage, heating, radioactivity, and shielding applications over the incident neutron energy range from 1.0E-11 to 150 MeV. The discussion here is divided into the region below and above 20 MeV.

INCIDENT NEUTRON ENERGIES < 20 MeV

Below 20 MeV the evaluation is based completely on the ENDF/B-VI.5 (Release 2) evaluation by Larson, C. Perey, Hetrich, and Fu.

INCIDENT NEUTRON ENERGIES > 20 MeV

The ENDF/B-VI Release 2 evaluation extends to 20 MeV and includes cross sections and energy-angle data for all significant reactions. The present evaluation utilizes a more compact composite reaction spectrum representation above 20 MeV in order to reduce the length of the file. No essential data for applications is lost with this representation.

The evaluation above 20 MeV utilizes MF=6, MT=5 to represent all reaction data. Production cross sections and emission spectra are given for neutrons, protons, deuterons, tritons, alpha particles, gamma rays, and all residual nuclides produced ($A>5$) in the reaction chains. To summarize, the ENDF sections with non-zero data above $E_n = 20$ MeV are:

MF=3 MT= 1 Total Cross Section
MT= 2 Elastic Scattering Cross Section
MT= 3 Nonelastic Cross Section
MT= 5 Sum of Binary (n,n') and (n,x) Reactions

MF=4 MT= 2 Elastic Angular Distributions

MF=6 MT= 5 Production Cross Sections and Energy-Angle Distributions for Emission Neutrons, Protons, Deuterons, Tritons, and Alphas; and Angle-Integrated Spectra for Gamma Rays and Residual Nuclei That Are Stable Against Particle Emission

The evaluation is based on nuclear model calculations that have been benchmarked to experimental data, especially for n + Ni58 and p + Ni58 reactions (Ch97). We use the GNASH code system (Yo92), which utilizes Hauser-Feshbach statistical, preequilibrium and direct-reaction theories. Spherical optical model calculations are used to obtain particle transmission coefficients for the Hauser-Feshbach calculations, as well as for the elastic neutron angular distributions.

Cross sections and spectra for producing individual residual nuclei are included for reactions. The energy-angle-correlations for all outgoing particles are based on Kalbach systematics (Ka88).

A model was developed to calculate the energy distributions of

all recoil nuclei in the GNASH calculations (Ch96). The recoil energy distributions are represented in the laboratory system in MT=5, MF=6, and are given as isotropic in the lab system. All other data in MT=5, MF=6 are given in the center-of-mass system. This method of representation utilizes the LCT=3 option approved at the November, 1996, CSEWG meeting.

Preequilibrium corrections were performed in the course of the GNASH calculations using the exciton model of Kalbach (Ka77, Ka85), validated by comparison with calculations using Feshbach, Kerman, Koonin (FKK) theory [Ch93]. Discrete level data from nuclear data sheets were matched to continuum level densities using the formulation of Gilbert and Cameron (Gi65) and pairing and shell parameters from the Cook (Co67) analysis. Neutron and charged-particle transmission coefficients were obtained from the optical potentials, as discussed below. Gamma-ray transmission coefficients were calculated using the Kopecky-Uhl model (Ko90).

SOME NI-SPECIFIC INFORMATION CONCERNING THE EVAL.

The neutron total cross section was evaluated based on the least-squares method taking account of the experimental data (Du67, Bo71, St71, Sm79, Fe80, Pe82, Ha82a, Di97). The data for natural Ni (Di97) was also used because there was not enough data for Ni-60 above 20 MeV. The data for natural Ni were transformed to the Ni-60 cross section according to $A^{*(2/3)}$ law. Result of this estimation was used as the evaluated total cross section data above 20 MeV.

The evaluated total cross section data (1 to 250 MeV), s-wave strength function (Mu81) and elastic scattering angular distribution data (Bo71, Gu85, Tu73, Ya79) were used to obtain the neutron optical potential parameters. The parameter estimation was carried out based on Marquart-Bayesian approach (Sm91), where ECIS95 code (Ra96) was used for the optical model calculation. We have employed the energy dependence of the optical potential similar to Delaroche's work (De89). The initial potential parameters were adopted from Koning and Delaroche (Ko97). A total of 7 parameters concerning the central potential depth were estimated with associated covariance matrix, while the geometrical parameters were fixed to the result of a similar search for n + Ni-58. Presently obtained potential was used for the calculation of neutron transmission coefficients and DWBA cross sections in the energy region above 20 MeV. Below 20 MeV, the Harper neutron potential (Ha82b) was used for the calculation of transmission coefficients.

The proton optical potential was also searched to obtain a good description of proton-total reaction cross section as predicted by Wellisch-Axen systematic (We96) above 50 MeV. The parameter estimation was carried out by the Marquart-Bayesian approach similar to the neutron OMP, but trying to seek the best parameter to reproduce the reaction cross sections compiled by Carlson (Ca96) and Wellisch values. The experimental data in Carlson (Ca96) was scaled for Ni-60 according to $A^{**(2/3)}$ law. In this search, the geometrical parameters were fixed to be same as the neutron potential. The present potential gives a good description of the proton total reaction cross section from 10 MeV to 250 MeV. However, after some trial and error to reproduce both the elastic

28060 = TARGET 1000Z+A (if A=0 then elemental)

1 = PROJECTILE 1000Z+A

Nonelastic, elastic, and Production cross sections for A<5 projectiles in barns:

| Energy | nonelas | elastic | neutron | proton | deuteron | triton | helium3 | alpha | gamma |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.000E+01 | 1.348E+00 | 1.033E+00 | 1.822E+00 | 3.878E-01 | 2.882E-02 | 8.594E-04 | 0.000E+00 | 8.832E-02 | 3.361E+00 |
| 2.200E+01 | 1.317E+00 | 1.031E+00 | 1.798E+00 | 4.084E-01 | 3.294E-02 | 1.430E-03 | 0.000E+00 | 9.432E-02 | 3.573E+00 |
| 2.400E+01 | 1.280E+00 | 1.060E+00 | 1.770E+00 | 4.348E-01 | 3.860E-02 | 1.993E-03 | 0.000E+00 | 9.866E-02 | 3.629E+00 |
| 2.600E+01 | 1.245E+00 | 1.093E+00 | 1.784E+00 | 4.688E-01 | 4.299E-02 | 2.639E-03 | 0.000E+00 | 1.015E-01 | 3.527E+00 |
| 2.800E+01 | 1.212E+00 | 1.160E+00 | 1.815E+00 | 5.043E-01 | 4.800E-02 | 3.269E-03 | 0.000E+00 | 1.032E-01 | 3.367E+00 |
| 3.000E+01 | 1.182E+00 | 1.225E+00 | 1.857E+00 | 5.395E-01 | 5.231E-02 | 3.847E-03 | 0.000E+00 | 1.047E-01 | 3.166E+00 |
| 3.500E+01 | 1.120E+00 | 1.381E+00 | 1.934E+00 | 6.187E-01 | 5.984E-02 | 5.056E-03 | 0.000E+00 | 1.110E-01 | 2.775E+00 |
| 4.000E+01 | 1.073E+00 | 1.498E+00 | 1.957E+00 | 7.113E-01 | 6.493E-02 | 6.000E-03 | 0.000E+00 | 1.172E-01 | 2.635E+00 |
| 4.500E+01 | 1.039E+00 | 1.587E+00 | 2.006E+00 | 8.127E-01 | 6.812E-02 | 6.792E-03 | 0.000E+00 | 1.221E-01 | 2.556E+00 |
| 5.000E+01 | 1.015E+00 | 1.623E+00 | 2.089E+00 | 9.044E-01 | 7.140E-02 | 7.548E-03 | 0.000E+00 | 1.286E-01 | 2.496E+00 |
| 5.500E+01 | 9.979E-01 | 1.628E+00 | 2.179E+00 | 9.862E-01 | 7.242E-02 | 8.263E-03 | 0.000E+00 | 1.355E-01 | 2.445E+00 |
| 6.000E+01 | 9.847E-01 | 1.607E+00 | 2.255E+00 | 1.060E+00 | 7.534E-02 | 8.965E-03 | 0.000E+00 | 1.419E-01 | 2.410E+00 |
| 6.500E+01 | 9.732E-01 | 1.543E+00 | 2.329E+00 | 1.131E+00 | 7.776E-02 | 9.614E-03 | 0.000E+00 | 1.479E-01 | 2.348E+00 |
| 7.000E+01 | 9.622E-01 | 1.478E+00 | 2.380E+00 | 1.203E+00 | 7.918E-02 | 1.022E-02 | 0.000E+00 | 1.528E-01 | 2.190E+00 |
| 7.500E+01 | 9.512E-01 | 1.417E+00 | 2.423E+00 | 1.257E+00 | 8.118E-02 | 1.079E-02 | 0.000E+00 | 1.578E-01 | 2.157E+00 |
| 8.000E+01 | 9.397E-01 | 1.348E+00 | 2.482E+00 | 1.311E+00 | 8.266E-02 | 1.148E-02 | 0.000E+00 | 1.653E-01 | 2.114E+00 |
| 8.500E+01 | 9.279E-01 | 1.260E+00 | 2.534E+00 | 1.364E+00 | 8.331E-02 | 1.219E-02 | 0.000E+00 | 1.729E-01 | 2.032E+00 |
| 9.000E+01 | 9.158E-01 | 1.185E+00 | 2.571E+00 | 1.406E+00 | 8.449E-02 | 1.290E-02 | 0.000E+00 | 1.790E-01 | 2.001E+00 |
| 9.500E+01 | 9.034E-01 | 1.112E+00 | 2.607E+00 | 1.447E+00 | 8.588E-02 | 1.382E-02 | 0.000E+00 | 1.868E-01 | 1.982E+00 |
| 1.000E+02 | 8.910E-01 | 1.061E+00 | 2.633E+00 | 1.477E+00 | 8.684E-02 | 1.459E-02 | 0.000E+00 | 1.925E-01 | 1.955E+00 |
| 1.100E+02 | 8.664E-01 | 9.049E-01 | 2.673E+00 | 1.530E+00 | 8.839E-02 | 1.638E-02 | 0.000E+00 | 2.045E-01 | 1.916E+00 |
| 1.200E+02 | 8.426E-01 | 8.008E-01 | 2.692E+00 | 1.567E+00 | 8.986E-02 | 1.807E-02 | 0.000E+00 | 2.130E-01 | 1.867E+00 |
| 1.300E+02 | 8.202E-01 | 7.117E-01 | 2.716E+00 | 1.600E+00 | 9.028E-02 | 1.996E-02 | 0.000E+00 | 2.216E-01 | 1.818E+00 |
| 1.400E+02 | 7.993E-01 | 6.333E-01 | 2.708E+00 | 1.614E+00 | 9.079E-02 | 2.139E-02 | 0.000E+00 | 2.261E-01 | 1.772E+00 |
| 1.500E+02 | 7.798E-01 | 5.768E-01 | 2.698E+00 | 1.630E+00 | 9.103E-02 | 2.297E-02 | 0.000E+00 | 2.298E-01 | 1.691E+00 |

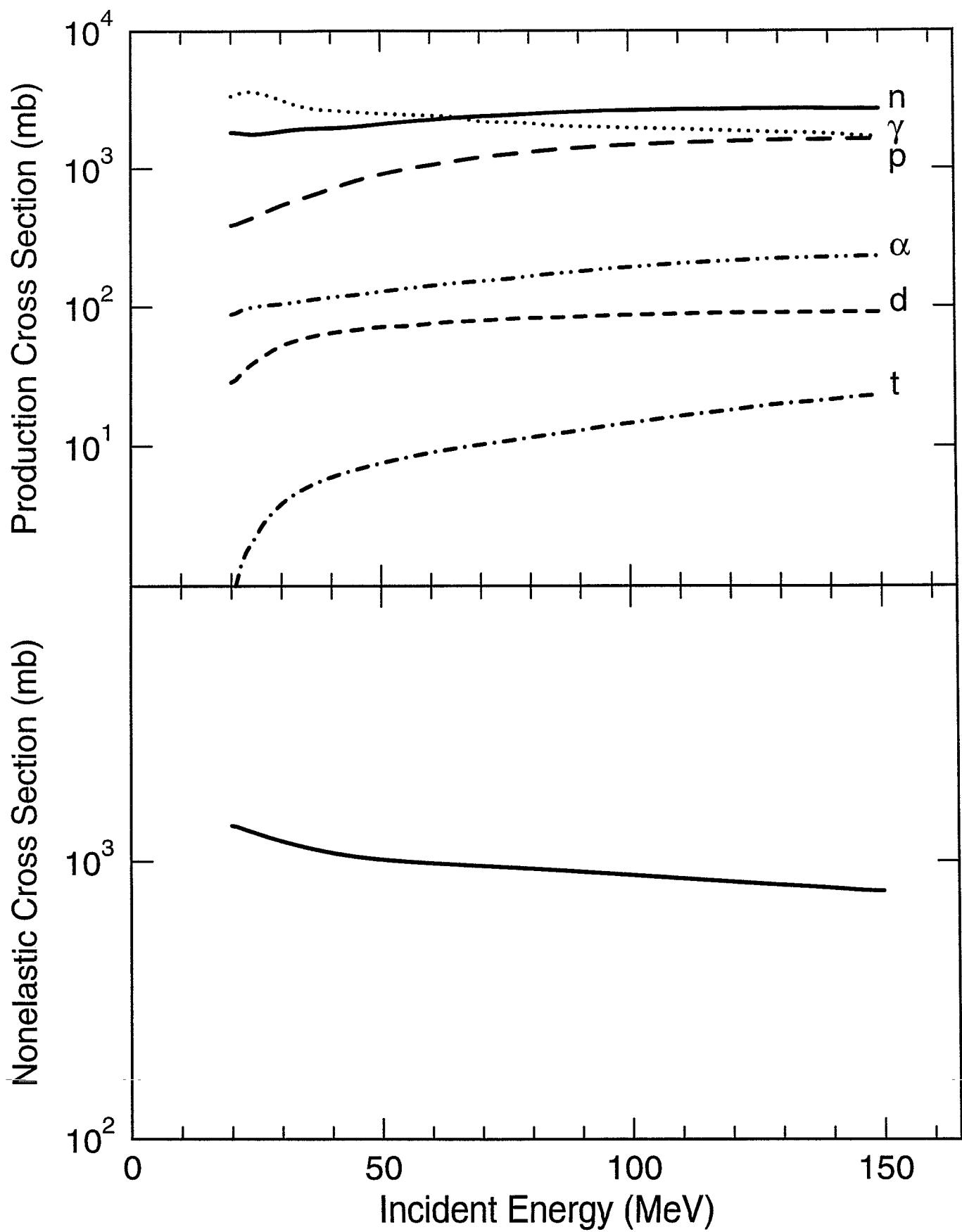
28060 = TARGET 1000Z+A (if A=0 then elemental)

1 = PROJECTILE 1000Z+A

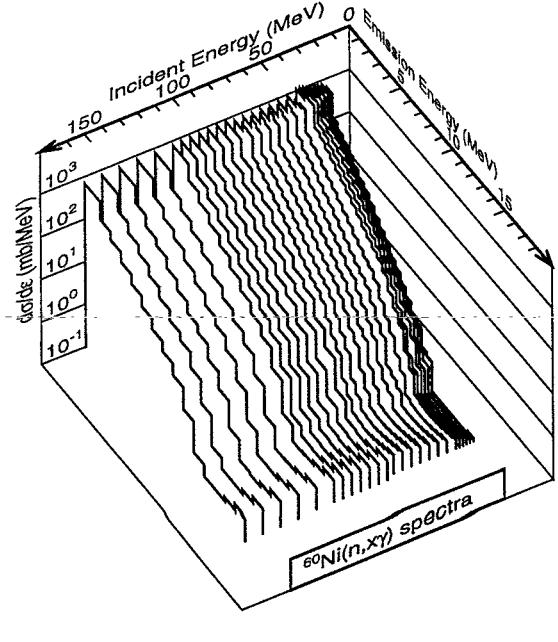
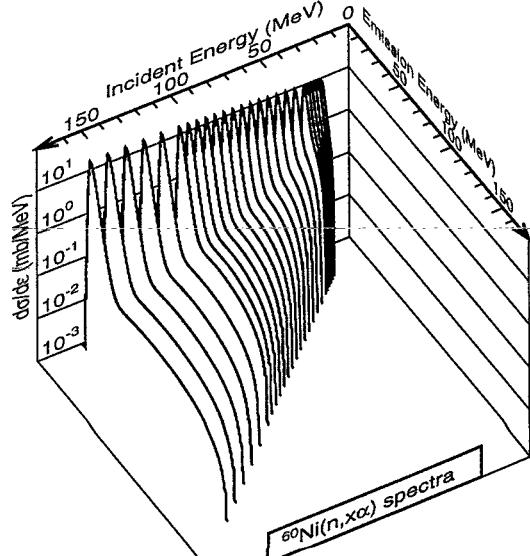
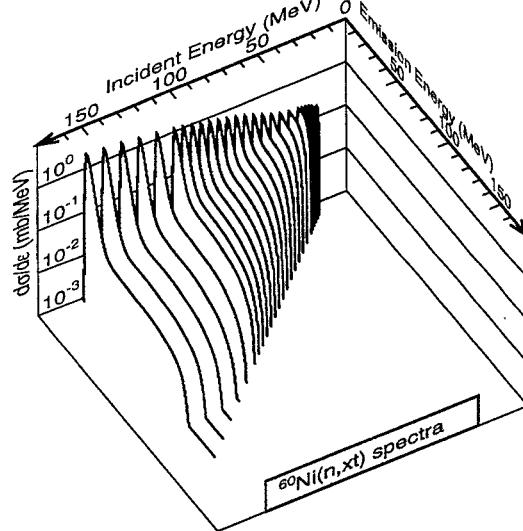
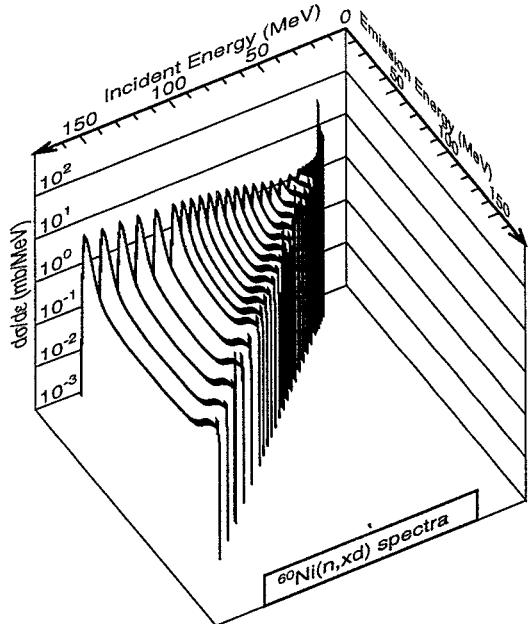
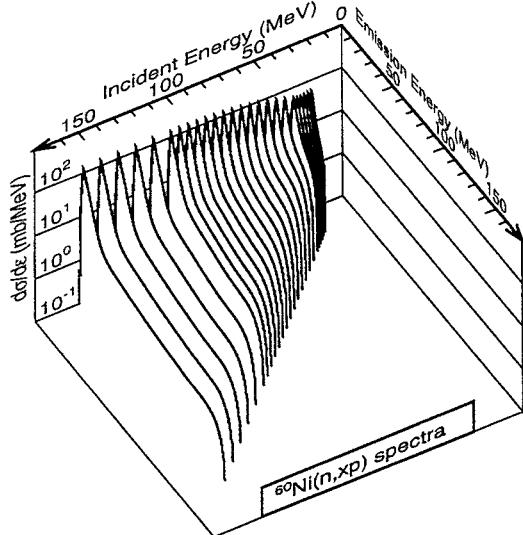
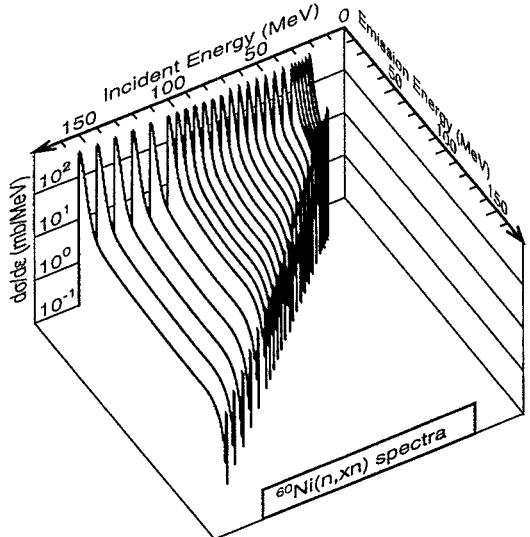
Kerma coefficients in units of f.Gy.m^2:

| Energy | proton | deuteron | triton | helium3 | alpha | non-rec | elas-rec | TOTAL |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 2.000E+01 | 4.010E-01 | 4.122E-02 | 7.883E-04 | 0.000E+00 | 1.398E-01 | 9.303E-02 | 2.340E-02 | 6.993E-01 |
| 2.200E+01 | 4.552E-01 | 5.248E-02 | 1.515E-03 | 0.000E+00 | 1.534E-01 | 9.902E-02 | 2.272E-02 | 7.844E-01 |
| 2.400E+01 | 5.092E-01 | 6.842E-02 | 2.356E-03 | 0.000E+00 | 1.642E-01 | 1.036E-01 | 2.438E-02 | 8.721E-01 |
| 2.600E+01 | 5.681E-01 | 8.320E-02 | 3.476E-03 | 0.000E+00 | 1.726E-01 | 1.075E-01 | 2.528E-02 | 9.602E-01 |
| 2.800E+01 | 6.345E-01 | 1.015E-01 | 4.728E-03 | 0.000E+00 | 1.788E-01 | 1.108E-01 | 2.629E-02 | 1.057E+00 |
| 3.000E+01 | 7.077E-01 | 1.200E-01 | 6.035E-03 | 0.000E+00 | 1.839E-01 | 1.138E-01 | 2.673E-02 | 1.158E+00 |
| 3.500E+01 | 9.039E-01 | 1.648E-01 | 9.425E-03 | 0.000E+00 | 1.997E-01 | 1.222E-01 | 2.648E-02 | 1.427E+00 |
| 4.000E+01 | 1.126E+00 | 2.099E-01 | 1.272E-02 | 0.000E+00 | 2.155E-01 | 1.299E-01 | 2.506E-02 | 1.720E+00 |
| 4.500E+01 | 1.363E+00 | 2.498E-01 | 1.584E-02 | 0.000E+00 | 2.292E-01 | 1.373E-01 | 2.346E-02 | 2.019E+00 |
| 5.000E+01 | 1.603E+00 | 2.904E-01 | 1.882E-02 | 0.000E+00 | 2.453E-01 | 1.450E-01 | 2.157E-02 | 2.325E+00 |
| 5.500E+01 | 1.848E+00 | 3.153E-01 | 2.159E-02 | 0.000E+00 | 2.619E-01 | 1.522E-01 | 1.977E-02 | 2.619E+00 |
| 6.000E+01 | 2.086E+00 | 3.522E-01 | 2.423E-02 | 0.000E+00 | 2.776E-01 | 1.591E-01 | 1.814E-02 | 2.918E+00 |
| 6.500E+01 | 2.327E+00 | 3.865E-01 | 2.664E-02 | 0.000E+00 | 2.926E-01 | 1.657E-01 | 1.641E-02 | 3.215E+00 |
| 7.000E+01 | 2.568E+00 | 4.134E-01 | 2.886E-02 | 0.000E+00 | 3.058E-01 | 1.713E-01 | 1.499E-02 | 3.503E+00 |
| 7.500E+01 | 2.794E+00 | 4.457E-01 | 3.088E-02 | 0.000E+00 | 3.187E-01 | 1.754E-01 | 1.382E-02 | 3.779E+00 |
| 8.000E+01 | 3.015E+00 | 4.728E-01 | 3.275E-02 | 0.000E+00 | 3.362E-01 | 1.802E-01 | 1.274E-02 | 4.049E+00 |
| 8.500E+01 | 3.234E+00 | 4.905E-01 | 3.452E-02 | 0.000E+00 | 3.536E-01 | 1.843E-01 | 1.162E-02 | 4.308E+00 |
| 9.000E+01 | 3.437E+00 | 5.144E-01 | 3.619E-02 | 0.000E+00 | 3.688E-01 | 1.874E-01 | 1.071E-02 | 4.554E+00 |
| 9.500E+01 | 3.636E+00 | 5.364E-01 | 3.795E-02 | 0.000E+00 | 3.870E-01 | 1.905E-01 | 9.892E-03 | 4.798E+00 |
| 1.000E+02 | 3.831E+00 | 5.584E-01 | 3.946E-02 | 0.000E+00 | 4.012E-01 | 1.926E-01 | 9.312E-03 | 5.032E+00 |
| 1.100E+02 | 4.204E+00 | 5.931E-01 | 4.245E-02 | 0.000E+00 | 4.309E-01 | 1.964E-01 | 7.788E-03 | 5.474E+00 |
| 1.200E+02 | 4.561E+00 | 6.337E-01 | 4.480E-02 | 0.000E+00 | 4.544E-01 | 1.967E-01 | 6.800E-03 | 5.898E+00 |
| 1.300E+02 | 4.909E+00 | 6.489E-01 | 4.653E-02 | 0.000E+00 | 4.779E-01 | 2.025E-01 | 5.989E-03 | 6.290E+00 |
| 1.400E+02 | 5.240E+00 | 6.849E-01 | 4.703E-02 | 0.000E+00 | 4.930E-01 | 2.076E-01 | 5.299E-03 | 6.678E+00 |
| 1.500E+02 | 5.564E+00 | 7.102E-01 | 4.759E-02 | 0.000E+00 | 5.068E-01 | 2.112E-01 | 4.810E-03 | 7.044E+00 |

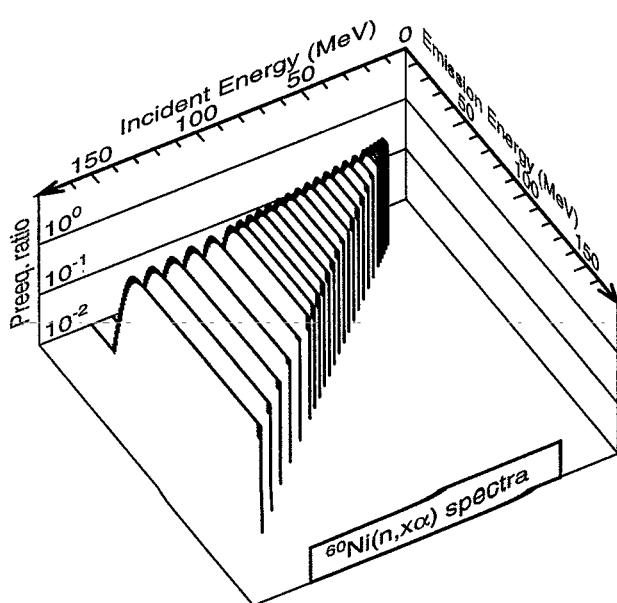
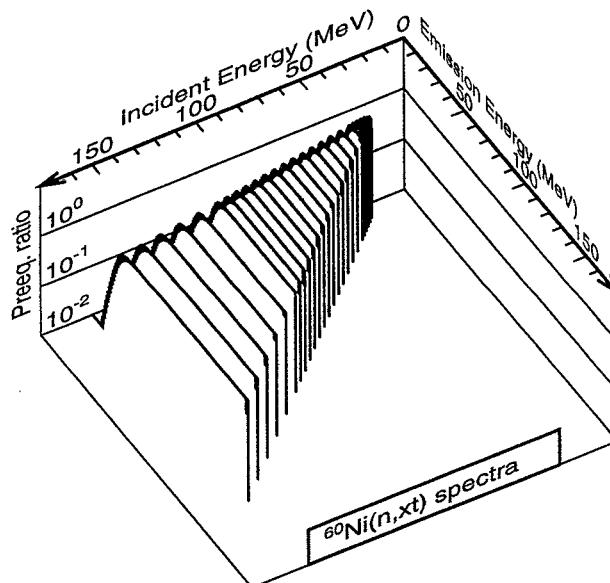
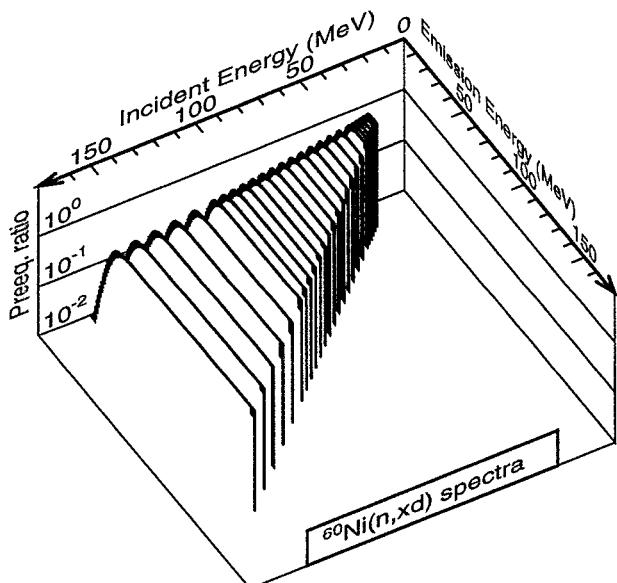
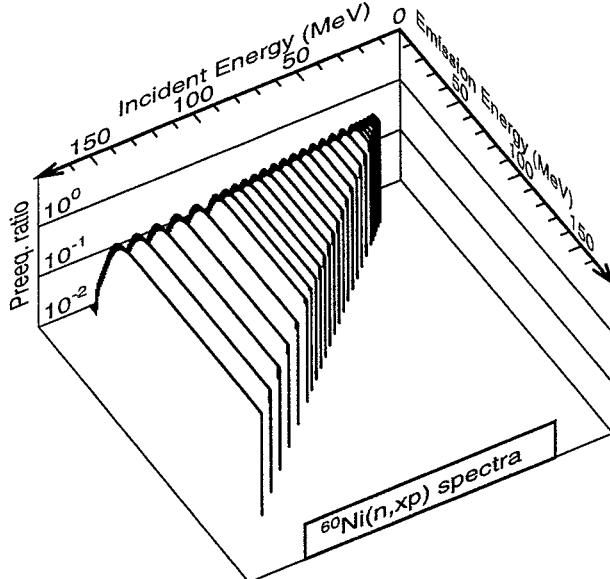
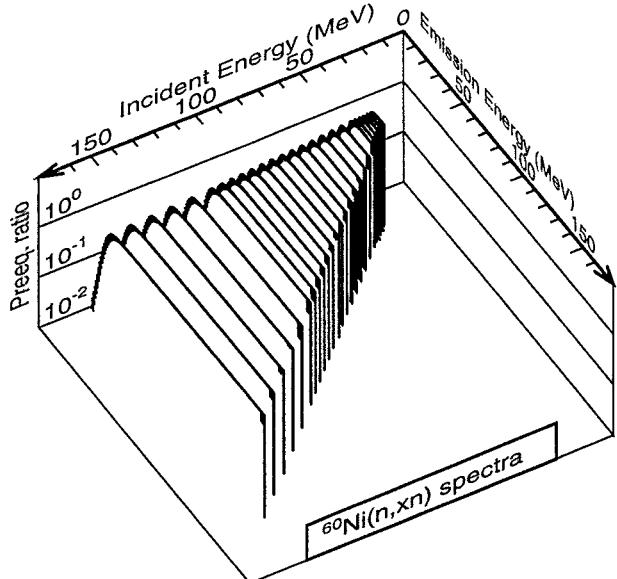
$n + {}^{60}\text{Ni}$ nonelastic and production cross sections



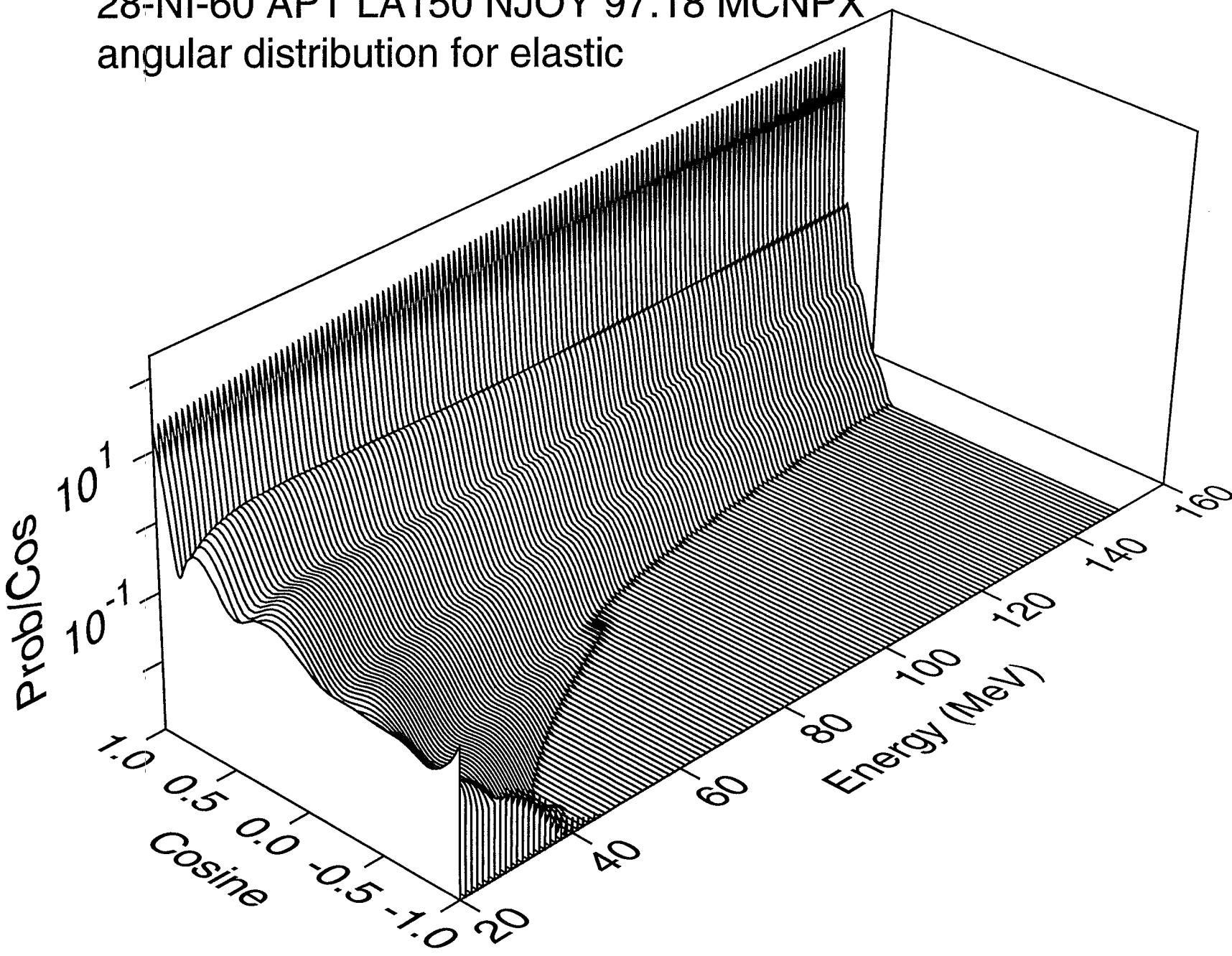
$n + {}^{60}\text{Ni}$ angle-integrated emission spectra



$n + {}^{60}\text{Ni}$ Kalbach preequilibrium ratios

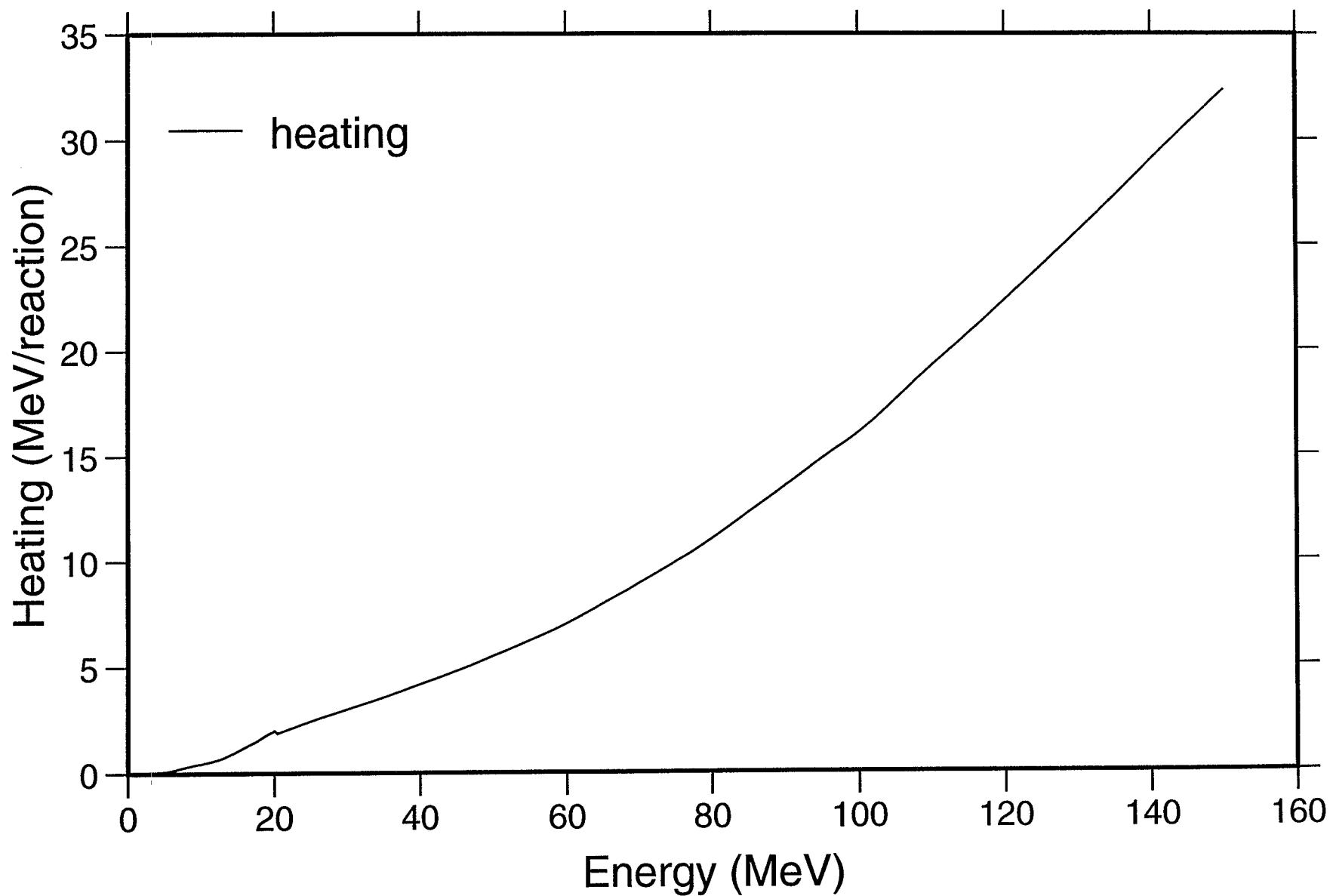


28-NI-60 APT LA150 NJOY 97.18 MCNPX
angular distribution for elastic



28-NI-60 APT LA150 NJOY 97.18 MCNPX

Heating



28-NI-60 APT LA150 NJOY 97.18 MCNPX

Damage

